PHYS 2211 Recitation 04

Jun 13–15

You should work in collaborative groups of 3–4, but each student must write up their own solution to the problem. Show all your work, and explain all your reasoning.

A wooden block of mass m is placed on a wooden wedge, which rests on a horizontal tabletop. The wedge has the shape of a 3-4-5 triangle, so that the inclined surface of the wedge makes an angle θ relative to the horizontal, satisfying the trigonometric identities:

 $\sin \theta = 3/5$ $\cos \theta = 4/5$ $\tan \theta = 3/4$



The coefficients of friction between the block and wedge are: $\mu_s = 0.500$ and $\mu_k = 0.200$.

TA Analysis: Each student should complete this portion of the worksheet individually, following along as the TA works the problem. The work you show here will be factored into your grade!

A. Will the block remain stationary, if placed on the wedge at rest? Justify your conclusion by constructing a free body diagram and applying Netwon's 2nd Law to the block.



Solution

B. A friend suggests that the block can be prevented from slipping down the wedge simply by pushing the wedge to the right at some constant speed v. He asserts that you can use the 2nd Law to determine the precise speed necessary. Is he correct? Why or why not?

"Constant speed" (and direction ...) implies zero acceleration - o this would again be an equilibrium situation, and the analysis above in Part A would again be applicable, This would not work

C. You decide instead that the block can be prevented from slipping by giving the wedge — and by association, the block – a constant rightward acceleration of some magnitude a. Explain why this would work, even if there were no friction whatsoever.

=DQ

Note that the acceleration would be honizontal, so the "best" Coordinate system would be honizontal trientical, fixed to the tabletop - In this coord system, component of N would cancel grav force = N would be bigger than it was in part A - horizontal component Nx would be an unbalanced component and could provide exactly the right amount of ax to Keep up with the wedge. Result: No accel for block relative to the wedge (No slippage...) D. Calculate the magnitude of acceleration a_0 that prevents the block from slipping along a *frictionless* wedge.

Student Analysis: Complete the worksheet in collaborative groups of 3–4, with each student writing up their own solution to the problem. Show all your work, and explain all your reasoning.

E. Allowing for friction, it should be possible to give the block and wedge an acceleration smaller than a_0 , while still not allowing the block to slip. In such a case, what will be the direction of the friction force? Is it static or kinetic friction?

when a was zero (Aut A) block slid down incline. when a was <+ 40>1, block was in equilibrium. This is between those acceleration binits so the tendency is for block to slide down wedge. If its not actually sliding, it must be that static friction is present, pointing upslopp

F. Construct a free body diagram for the block, in the situation where the minimum possible "safe" acceleration, a_{\min} , is being imparted to both objects. (*Hint:* choose your coordinate axes based on the direction of \vec{a} .)



G. Apply Newton's 2nd Law to determine the value for a_{\min} . Express your answer as a numerical multiple of g.

Vertical:
$$\langle +N\cos\theta \rangle + \langle +f_{5}\sin\theta \rangle + \langle -mg \rangle = 0$$

 $N\cos\theta + (u_{5}N)\sin\theta = mg$ $N = \frac{mg}{\cos\theta + u_{5}\sin\theta}$
horizontal: $\langle +N\sin\theta \rangle + \langle -f_{5}\cos\theta \rangle = m\langle +\Omega_{min} \rangle$ $(don't forget - there is horizontal accel, here's horizontal ac$

Checkpoint: Before continuing further, have the TA review your group's work so far.

H. It should also be possible to give the block and wedge an acceleration greater than a_0 while still not allowing the block to slip. How does the friction force in this situation differ from the friction force in Parts E–G? Can you think of a "quick and easy" way to convert your expression for a_{\min} into an expression for a_{\max} , the greatest possible acceleration for which the block will not slip?

For accel greater than
$$Q_0$$
, the component of the normal force Nx is not
"strong enough" by itself so block would tend to slip back", or "up the namp"
In limit where its almost slipping, is would be at its maximum value, pointing
downslope : is reverses direction as compared to Part G.
Note everywhere is appears, it is expressed as UsN (because we're at slipping limit)
Proplecement of every "Us" by "-Ms" would automatically reverse the direction
of F_x . Nothing else about problem changes, except $Q_{min} \rightarrow Q_{max}$
50: $Q_{min} = \begin{bmatrix} \sin \theta - M_s \cos \theta \\ \cos \theta + M_s \sin \theta \end{bmatrix} g \xrightarrow{we}{expect} Q_{max} = \begin{bmatrix} \sin \theta - (M_s) \cos \theta \\ \cos \theta + (M_s) \sin \theta \end{bmatrix} g = \begin{bmatrix} \sin \theta + M_s \cos \theta \\ \cos \theta - M_s \sin \theta \end{bmatrix} g$

I. Construct a free body diagram in the situation where the acceleration is a_{max} and use the 2nd Law to find an expression for a_{max} . Does this expression match the "quick and easy" expression that you found in the previous step?

$$\begin{aligned} & (\operatorname{key} - \operatorname{so} \operatorname{you} \operatorname{dorl} \operatorname{trask} \operatorname{youvelf} \operatorname{with} \operatorname{using} \operatorname{turt} \operatorname{kod} \operatorname{uouy} \operatorname{shorteut} \\ & (\operatorname{components} \operatorname{are}; N_{k} = \langle +N \sin \theta \rangle \quad N_{y} = \langle +N \cos \theta \rangle \\ & f_{x,x} = \langle +F_{x} \cos \theta \rangle \quad f_{x,y} = \langle -f_{x} \sin \theta \rangle \\ & (\operatorname{where} f_{x} = f_{x}, \operatorname{max} = \mathcal{M}_{x} N) \\ & (\operatorname{where} f_{x} = f_{x}, \operatorname{max} = \mathcal{M}_{x} N) \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{f}_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{f}_{x} \sin \theta) + \langle -\operatorname{mg} \rangle = 0 \\ & (\operatorname{where} f_{x} = f_{x} \sin \theta) + \langle -\operatorname{f}_{x} \sin \theta \rangle = \int_{\mathcal{M}} \operatorname{weithed} \operatorname{must} \operatorname{mu$$